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# Instabilities and Turbulence Studies on the Vertical Shock Tube



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May 13, 2021



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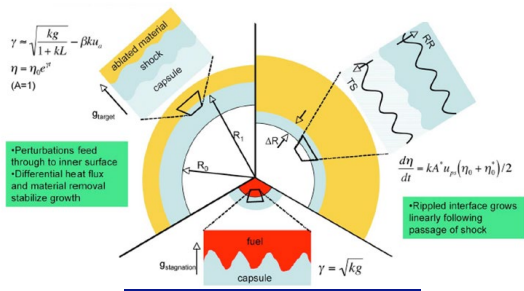


Erin Connor

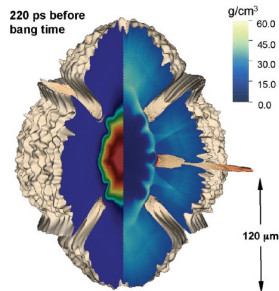


Antonio Martinez

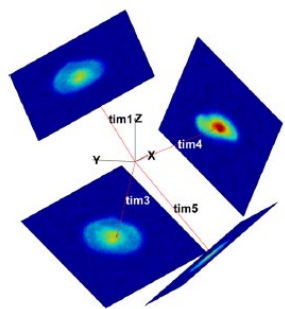
# Experimentally we find initial conditions affect how materials mix and turbulence develops, and these effects are not well captured in our simulations



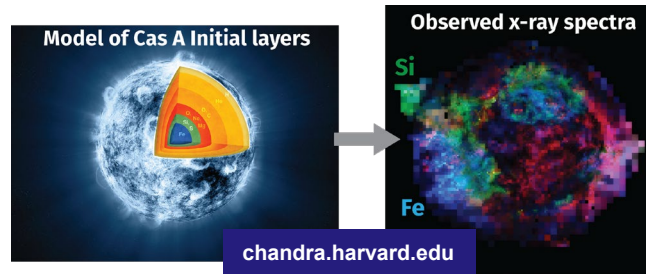
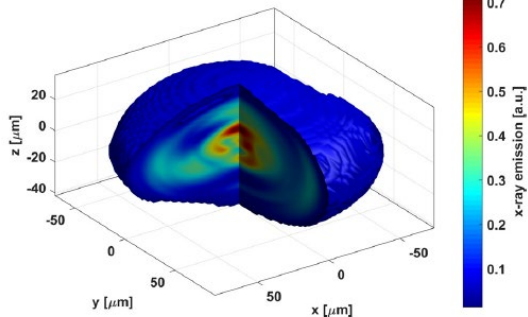
Loomis, E., et al. Phys. Plasmas 17 (2010)



Clark, D.S., et al. Physics of Plasmas 23 (2016)

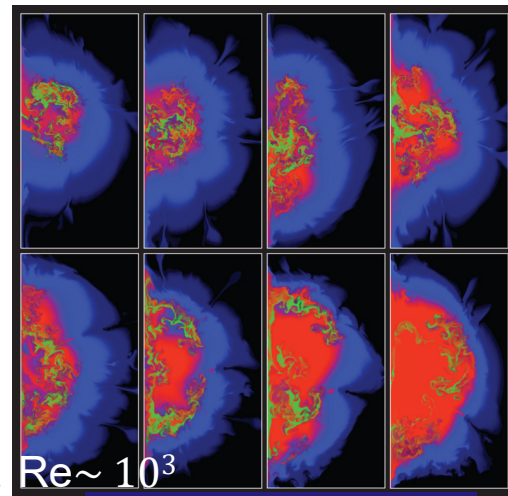


Volegov, P. L., et al. Journal of Applied Physics, 122 (2017)



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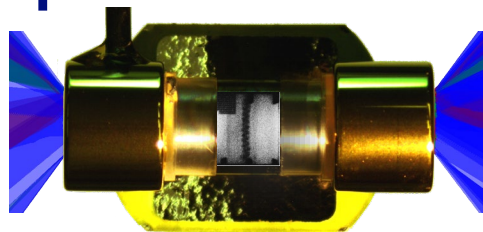
Simulation of IC effects on chemical structure



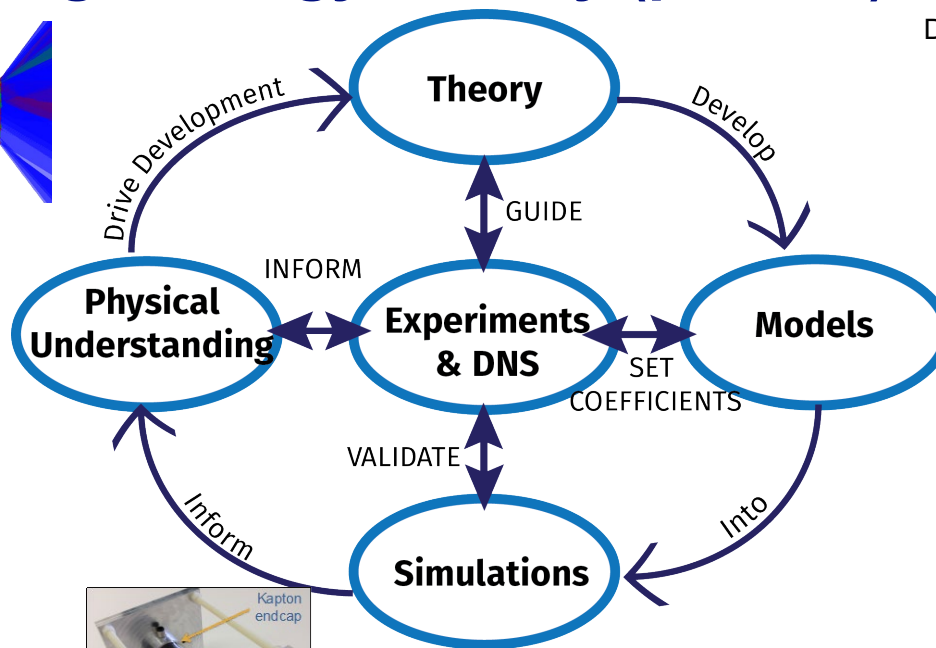
D Kasen et al. (2009) Nature



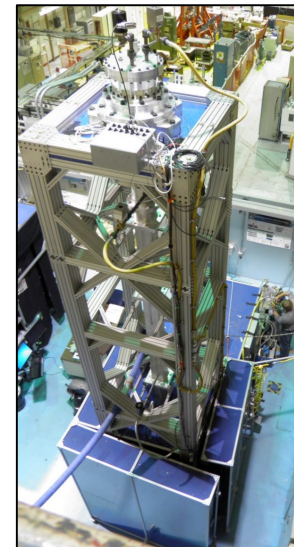
LANL is exploring this problem over a range of physical lengths and energy scales, from low-energy density (fluid) experiments to high-energy density (plasma) experiments



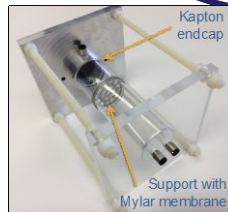
NIF Multi-interface work



DNS=Direct Numerical Simulations



Vertical Shock Tube (VST)



pRad turbulence experiments: MaRMITE

Lab-scale low-energy density experiments explore targeted physical processes to improve theoretical understanding, and help validate model implementation in codes



# Full understanding LANL's variable-density turbulence model, BHR, requires measurements of correlated velocity and density components

## Favre-averaged Reynolds Stress, $R_{ij}$

$$\begin{aligned} \frac{\partial (\bar{\rho} \tilde{R}_{ij})}{\partial t} + (\bar{\rho} \tilde{u}_k \tilde{R}_{ij})_{,k} &= [a_i \bar{P}_{,j} + a_j \bar{P}_{,i}] - \bar{\rho} [\tilde{R}_{ik} \tilde{u}_{j,k} + \tilde{R}_{jk} \tilde{u}_{i,k}] + \frac{C_\mu}{\sigma_k} (\bar{\rho} S_T \sqrt{K} \tilde{R}_{ij,k})_{,k} - C_{r3} \bar{\rho} \frac{\sqrt{K}}{S_D} \left( \tilde{R}_{ij} - \frac{1}{3} \tilde{R}_{kk} \delta_{ij} \right) \\ &\quad - C_{r1} [a_i \bar{P}_{,j} + a_j \bar{P}_{,i}] + C_{r2} \bar{\rho} [\tilde{R}_{ik} \tilde{u}_{j,k} + \tilde{R}_{jk} \tilde{u}_{i,k}] - C_{r2} \frac{2}{3} \bar{\rho} \tilde{R}_{mk} \tilde{u}_{m,k} \delta_{ij} + C_{r1} \frac{2}{3} a_k \bar{P}_{,k} \delta_{ij} - \bar{\rho} \frac{2}{3} \frac{K^{3/2}}{S_D} \delta_{ij} \end{aligned}$$

## Turbulent Mass Flux Transport

$$a_i \equiv -\overline{u_i''} = \overline{\rho' u_i'} / \bar{\rho}$$

$$\begin{aligned} \frac{\partial (\bar{\rho} a_i)}{\partial t} + (\bar{\rho} \tilde{u}_k a_i)_{,k} &= b \tilde{P}_{,i} - \tilde{R}_{ik} \bar{\rho}_{,k} - \bar{\rho} a_k \tilde{u}_{i,k} + \bar{\rho} (a_k a_i)_{,k} \\ &\quad + \bar{\rho} \frac{C_\mu}{\sigma_a} \left( S_T \sqrt{K} a_{i,k} \right)_{,k} - C_{ap} b \tilde{P}_{,i} + C_{au} \bar{\rho} a_k \tilde{u}_{i,k} - C_{a1} \bar{\rho} \frac{\sqrt{K}}{S_D} a_i \end{aligned}$$

## Density-Specific Volume correlation

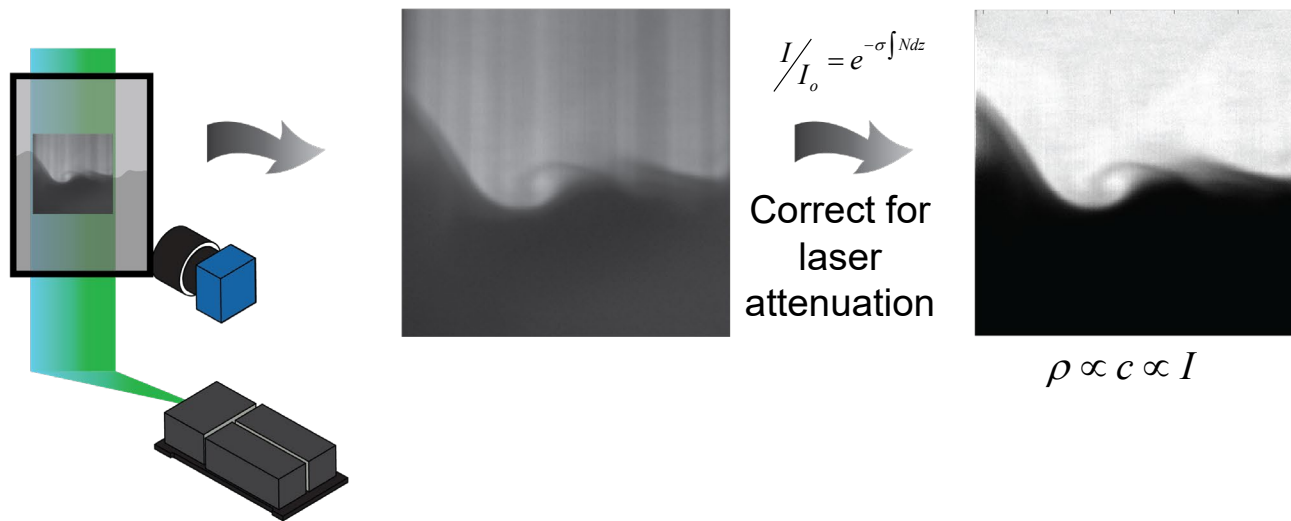
$$b = -\overline{\rho' (1/\rho)'} = -\overline{\rho' \tilde{u}_k} / \bar{\rho}$$

$$\frac{\partial (\bar{\rho} b)}{\partial t} + (\bar{\rho} b \tilde{u}_k)_{,k} = -2(b+1) a_k \bar{\rho}_{,k} + 2 \bar{\rho} a_k b_{,k} + \bar{\rho}^2 \frac{C_\mu}{\sigma_b} \left( \frac{1}{\bar{\rho}} S_T \sqrt{K} b_{,k} \right)_{,k} - C_{b1} \bar{\rho} \frac{\sqrt{K}}{S_D} b$$



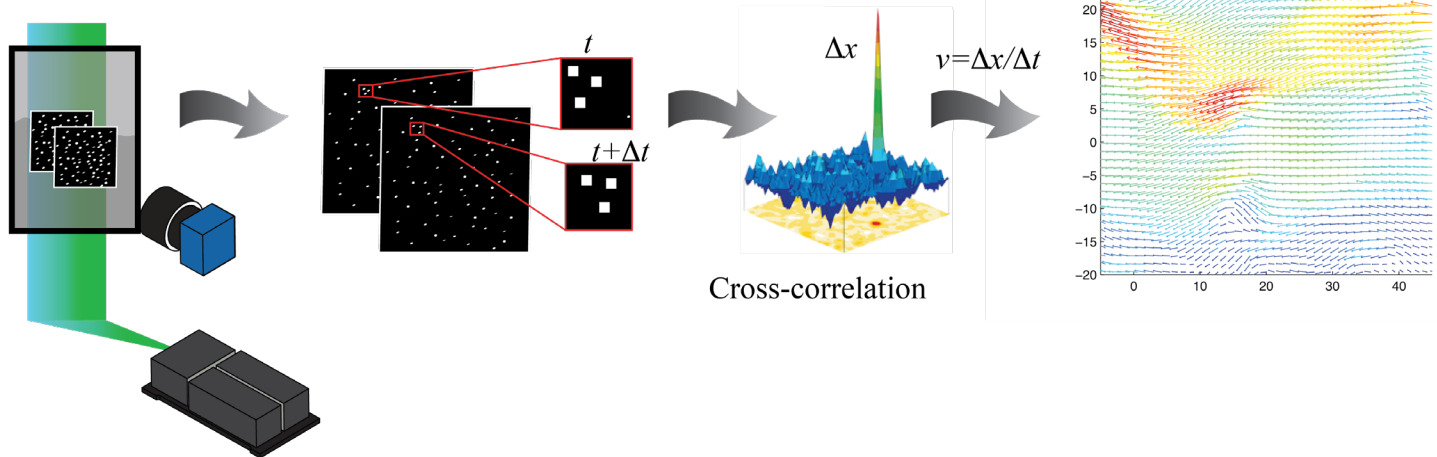


# Planar laser induced fluorescence (PLIF) uses a calibrated intensity signal to measure concentration and density fields



- Using optics laser light transformed into thin sheet ( ~ 1 mm thickness)
- Acetone tracer fluorescence centered at 405nm when excited by 266nm light.
- Fluorescence intensity is proportional to acetone concentration, allowing us to calibrate images to density

# Particle image velocimetry (PIV) uses correlation to track the displacement of particle groups

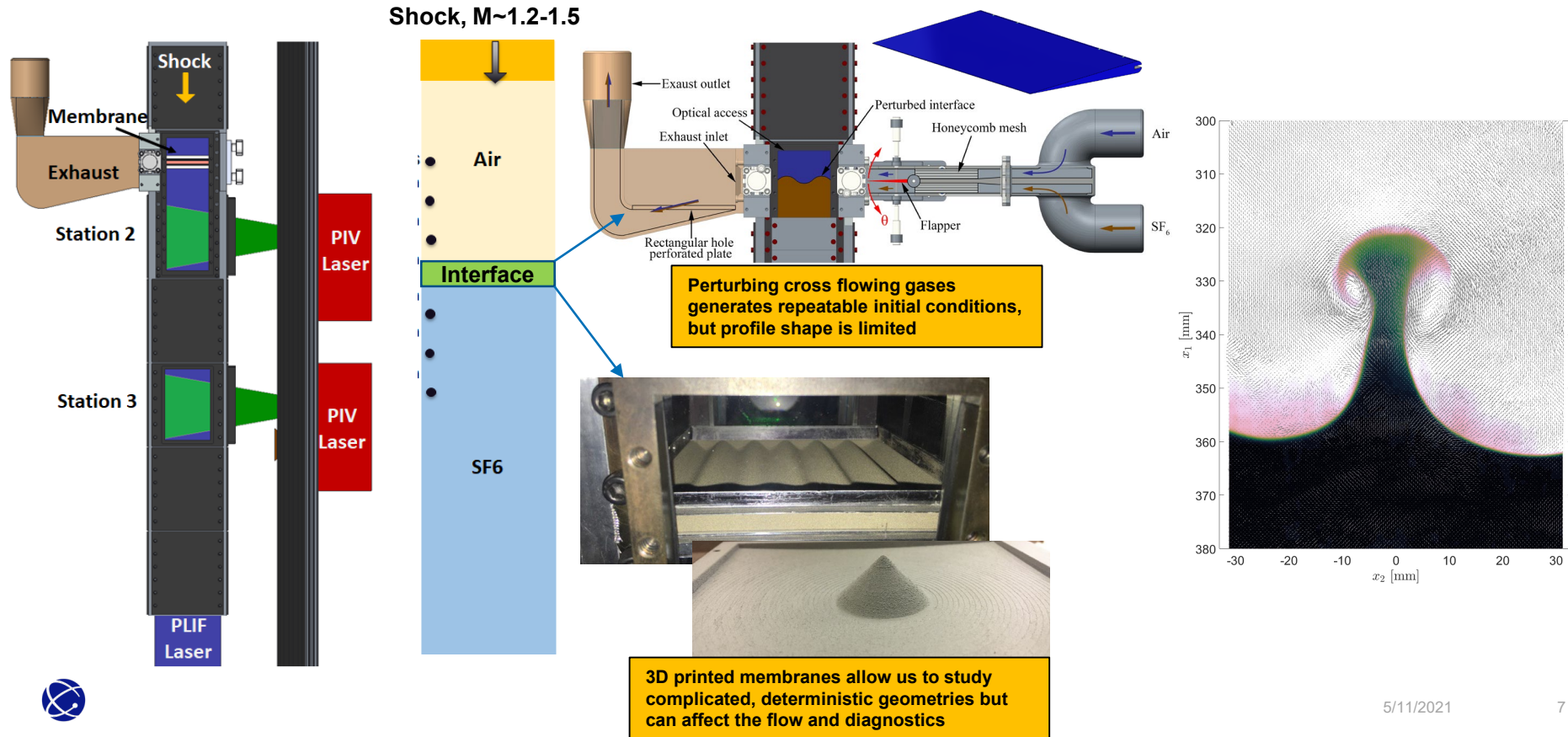


- Using optics laser light transformed into thin sheet ( ~ 1 mm thickness)
- Droplet tracers (such as olive oil ~ 1  $\mu\text{m}$  Ø) follow the flow field
- Illuminated particle positions imaged by dual frame camera.
- Average displacement of particles found by correlation.
- Local velocity calculated from local displacement and time interval between images

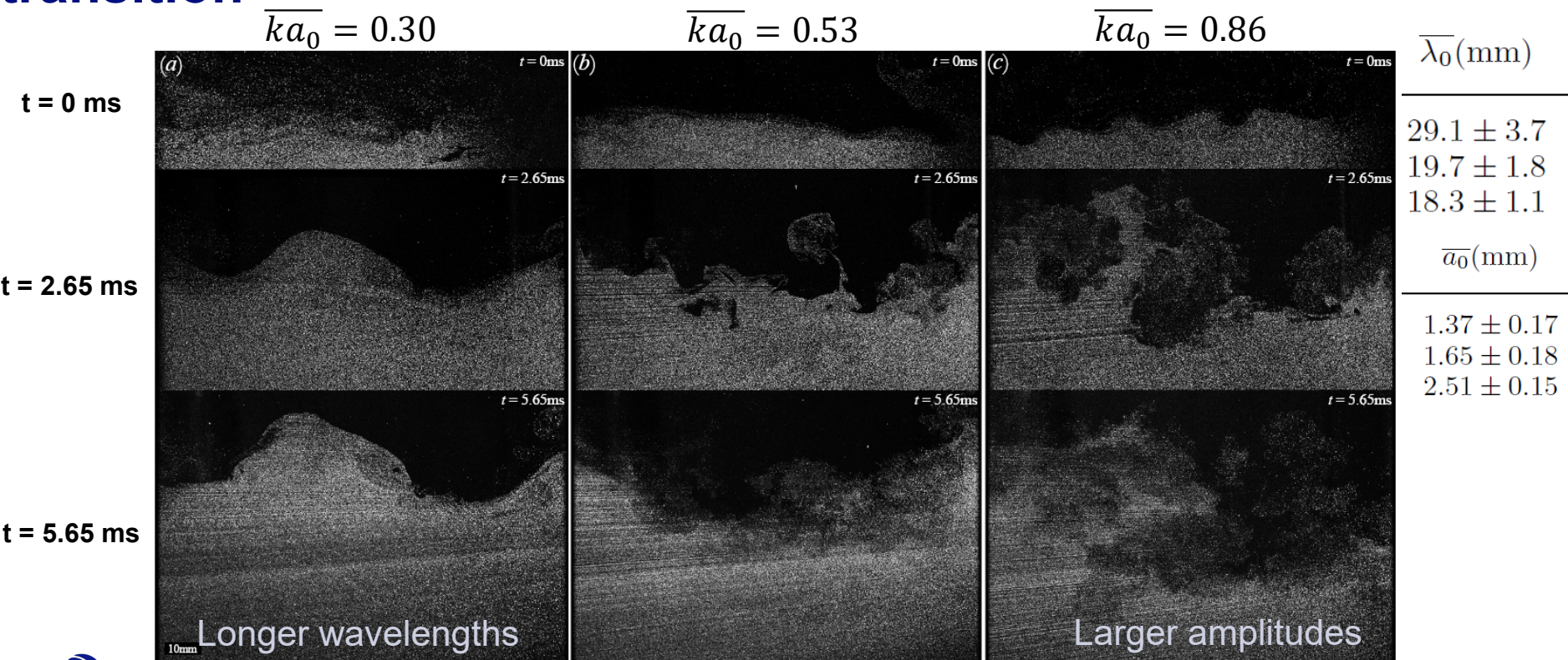




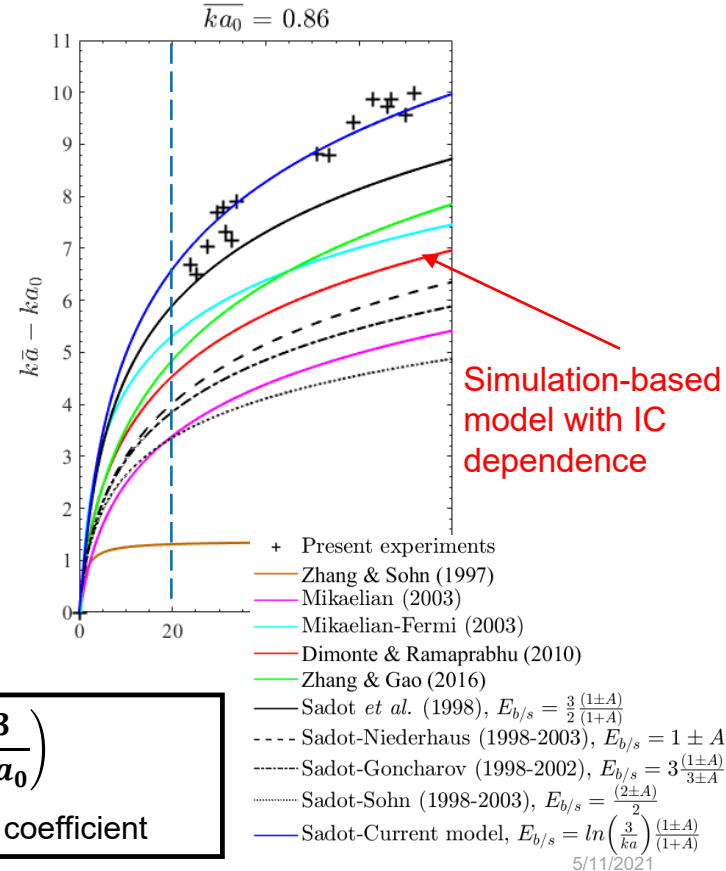
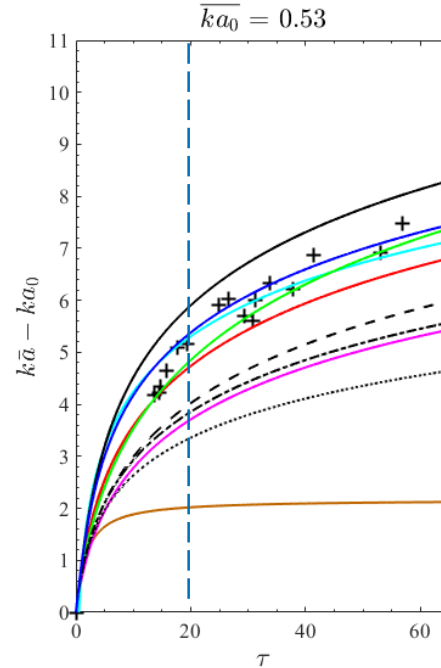
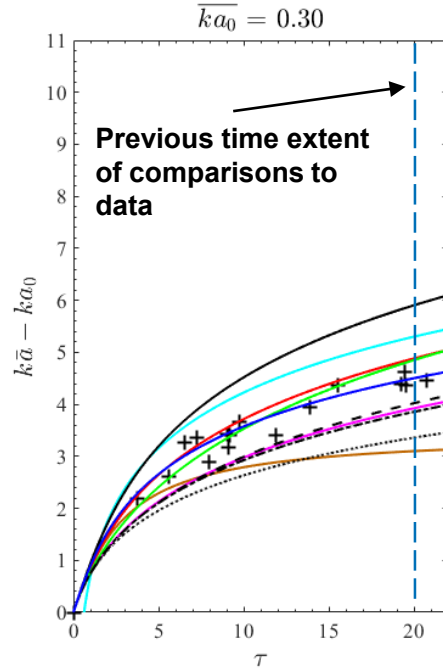
# The Vertical shock tube studies the effect of initial conditions on variable-density mixing under shock-driven conditions



# We found that increasing the perturbation frequency and amplitude of the initial conditions creates an earlier mixing transition



# We also found that we need to add a $ka_0$ dependence to the asymptotic component to match our experimental results



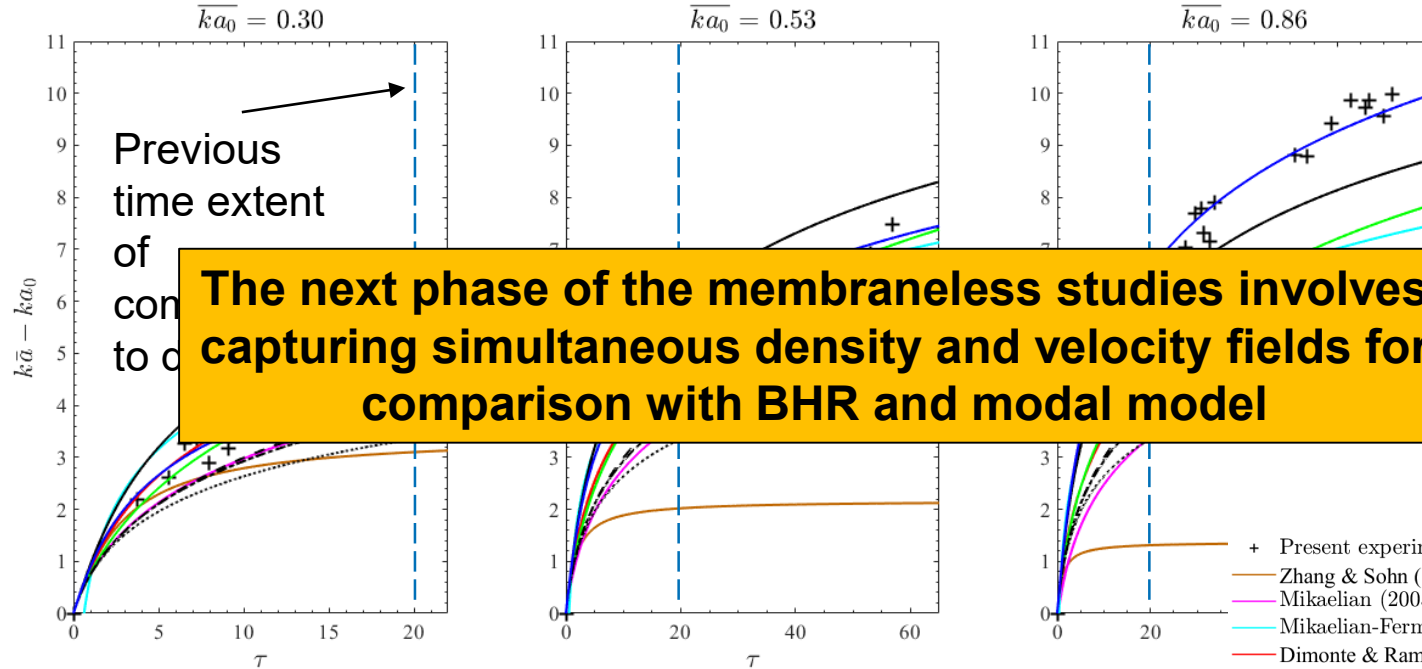
$$v_{b/s} = \frac{v_0(1 + v_0kt)}{1 + (1 \pm A)v_0kt + E_{b/s}v_0^2k^2t^2}$$

$$E_{b/s} = \frac{(1 \pm A)}{(1 + A)} \ln \left( \frac{3}{ka_0} \right)$$

Proposed IC-dependent coefficient



# We also found that we need to add a $ka_0$ dependence to the asymptotic component to match our experimental results



Simulation-based model with IC dependence

$$v_{b/s} = \frac{v_0(1 + v_0kt)}{1 + (1 \pm A)v_0kt + E_{b/s}v_0^2k^2t^2}$$

$$E_{b/s} = \frac{(1 \pm A)}{(1 + A)} \ln \left( \frac{3}{ka_0} \right)$$

Proposed IC-dependent coefficient

- + Present experiments
- Zhang & Sohn (1997)
- Mikaelian (2003)
- Mikaelian-Fermi (2003)
- Dimonte & Ramaprabhu (2010)
- Zhang & Gao (2016)
- Sadot *et al.* (1998),  $E_{b/s} = \frac{3}{2} \frac{(1 \pm A)}{(1 + A)}$
- Sadot-Niederhaus (1998-2003),  $E_{b/s} = 1 \pm A$
- Sadot-Goncharov (1998-2002),  $E_{b/s} = 3 \frac{(1 \pm A)}{3 \pm A}$
- Sadot-Sohn (1998-2003),  $E_{b/s} = \frac{(2 \pm A)}{2}$
- Sadot-Current model,  $E_{b/s} = \ln \left( \frac{3}{ka} \right) \frac{(1 \pm A)}{(1 + A)}$

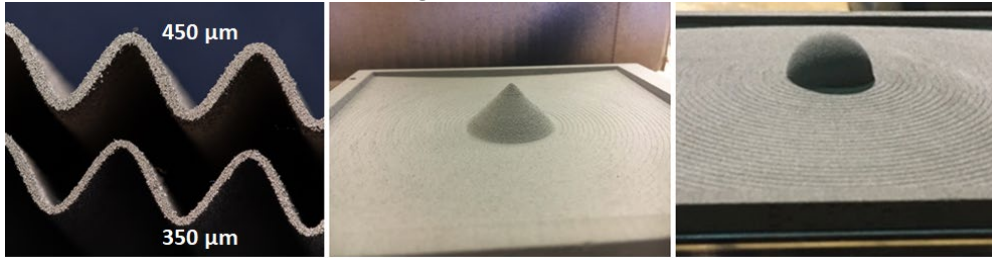




# We are pursuing methods of generating deterministic complex initial conditions

## Binder Jet:

Particle beds bounds together with binder



## Frames with fragile inner materials such as:

- Phylo dough
- Thin aluminum foil (0.9 μm and 2 μm?)
- Mylar

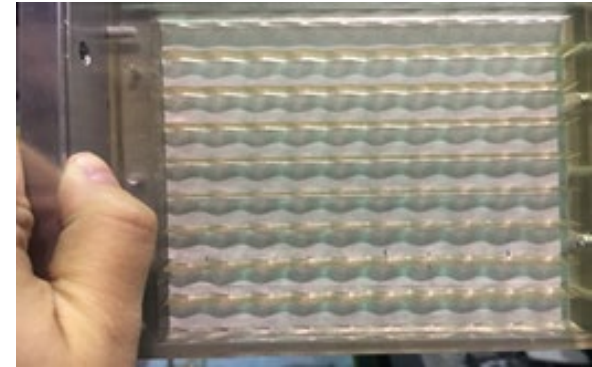
## SLA:

Resin vat hardened by laser



## FDM:

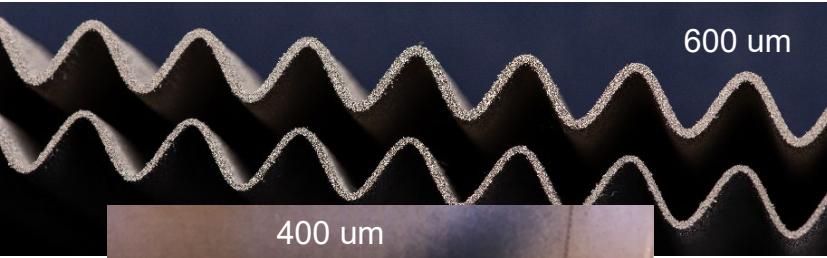
Materials heated and layered in semi-liquid state



**Majority of materials break poorly and reflections cause saturation of diagnostics**



# Binder jet membranes showed the most promise, are comprised of small ( $\sim 30\text{ }\mu\text{m}$ ) stainless steel particles

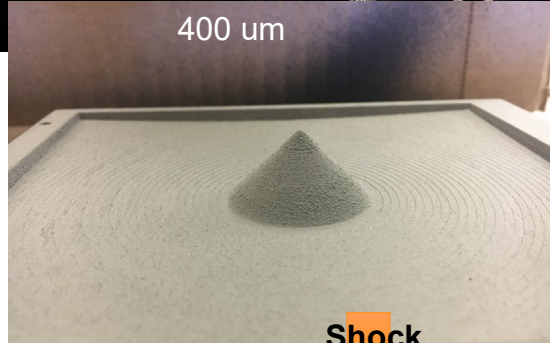


## Advantages:

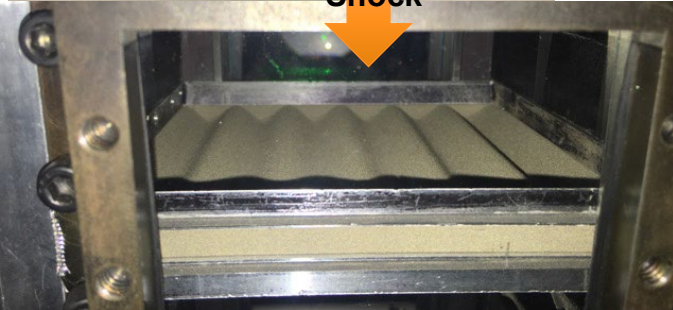
- Complex shapes
- In a green state, very fragile
- Minimal effect on diagnostics

## Disadvantages:

- 3D printing is not very precise, defects occur, membranes may not break reproducibly
- Particles are still large, and break into larger pieces
- Some pieces do flow with into optical view and degrade diagnostics
- In a green state, very fragile



Shock

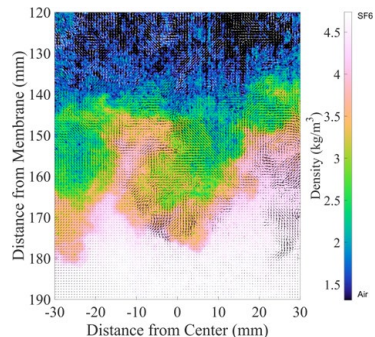


**Preliminary shots showed promising results, but breakup was found to be dependent on profile shape**

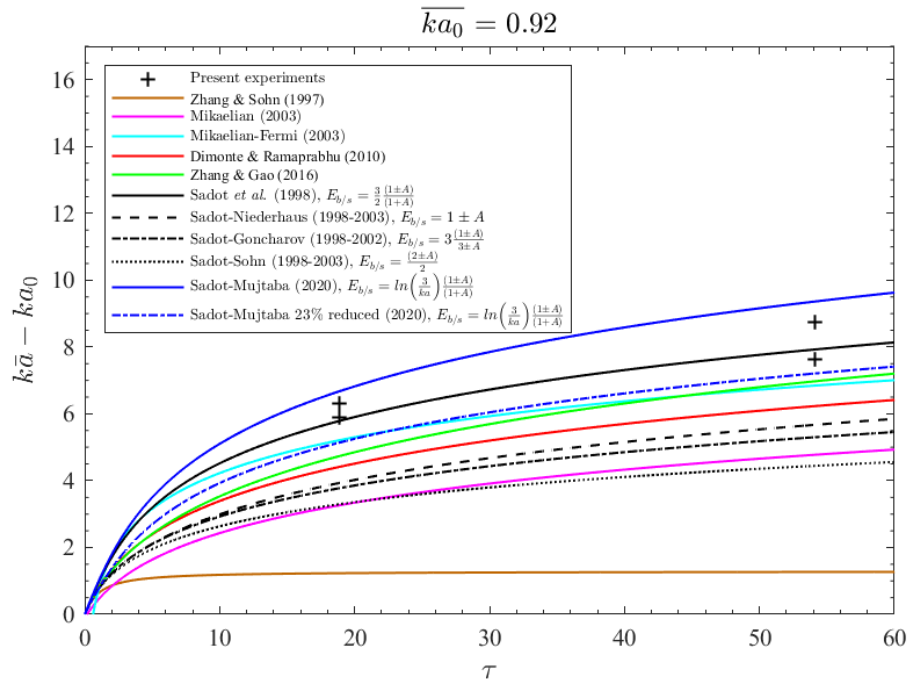
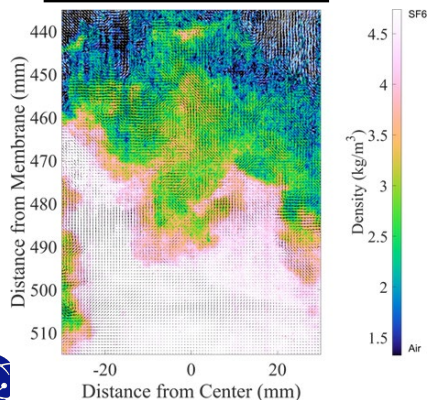


# Initial tests with $ka_0 = 0.92$ show large spike and bubble growth, and comparison with analytical models showed growth rate matched expectations

**Station 2 (t~1600 us)**

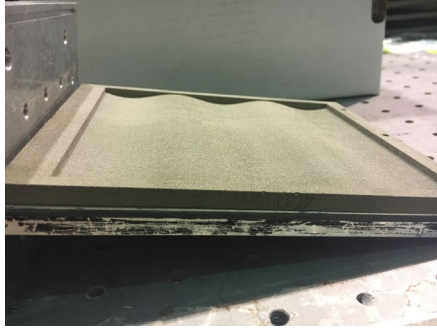


**Station 3 (t~4600 us)**

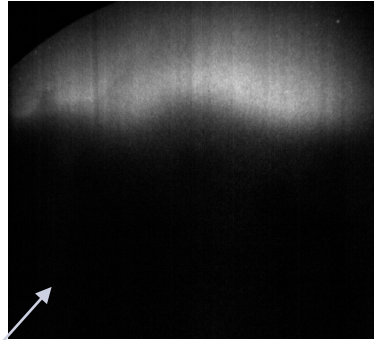




However, when we moved to  $ka = 0.24$ , with smaller amplitudes and longer wavelengths...



Station 2



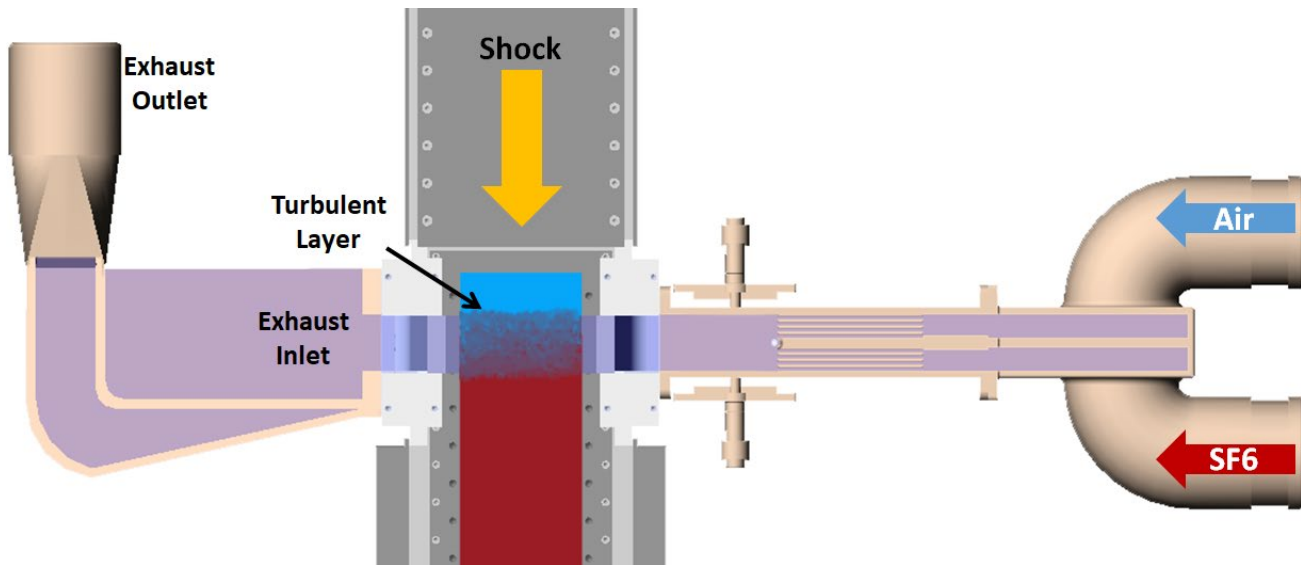
Station 2 looks 'clean'  
Station 3 is broken up

Station 3



**Long-wavelength membranes are  
breaking into larger pieces!**

# The VST is beginning work on studying shock-turbulence interactions in a variable-density setting

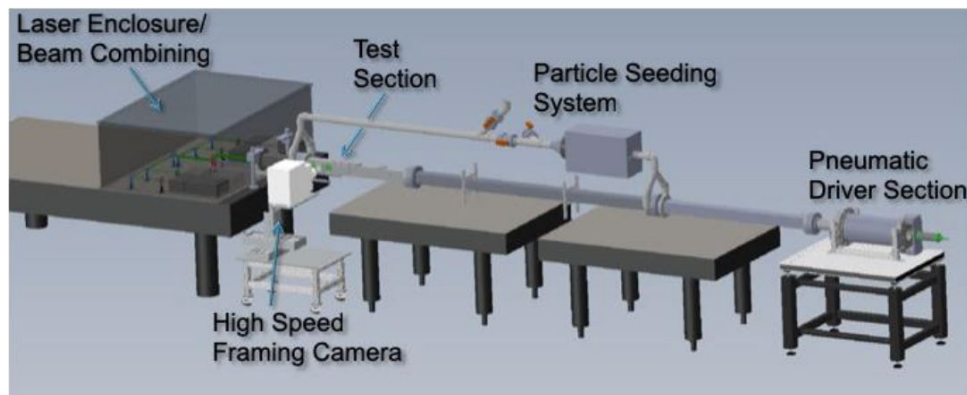


20210601ECR: Shocked Variable-Density Turbulence

**DNS simulations have studied this problem under limited conditions  
Experiments will be able to study regimes DNS cannot reach**



**Besides initial conditions, we also study particle drag and steady-state variable density turbulence...**

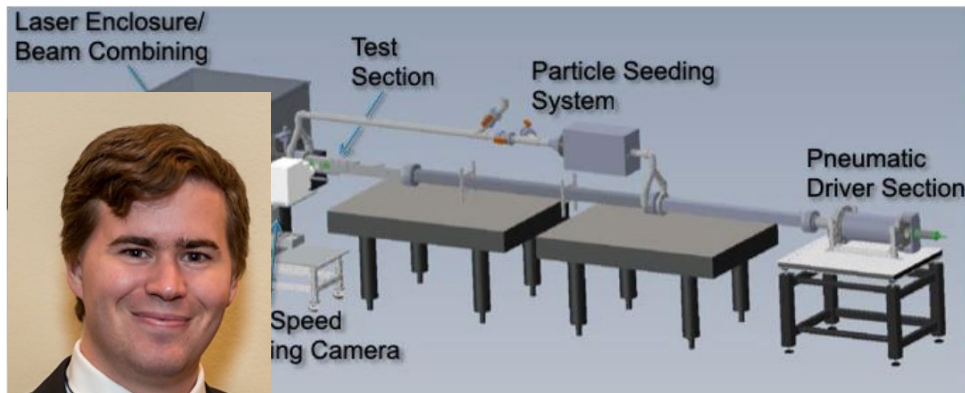


**Horizontal Shock Tube  
(HST)**

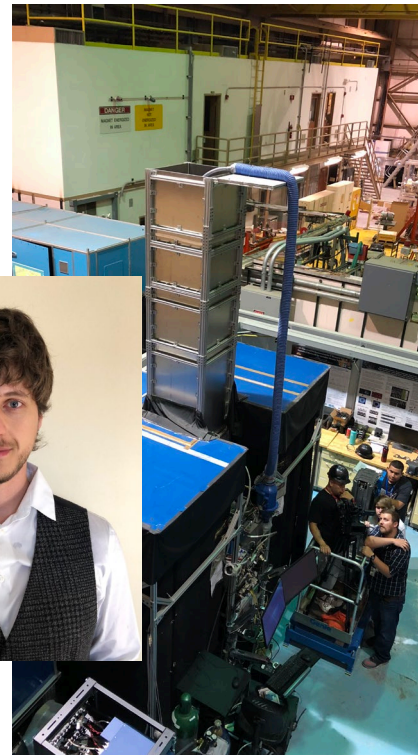


**Turbulent Mixing Tunnel  
(TMT)**

# Besides initial conditions, we also study particle drag and steady-state variable density turbulence...



**Horizontal Shock Tube  
(HST)**



**Turbulent Mixing Tunnel  
(TMT)**



# Thank you!

